

We examine the stresses which arise in an elastic half-space when the surface of the latter is suddenly heated, bearing in mind the rates of expansion-wave propagation in an elastic medium and the finite rate of heat propagation.

The dynamic problems of thermal elasticity were first treated in [1, 2], these papers devoted to the study of the stressed state resulting from the sudden heating of the plane surrounding an elastic half-space. These problems were subsequently again considered by Mura [3, 4] who apparently was unaware of [1, 2]. Further investigation of the dynamic problems of thermal elasticity are described in [5-9] and elsewhere. In each of these references the temperature field is described with the Fourier equation.

It is demonstrated in [10, 11] that for metals with a great temperature gradient there exists no classical relationship between the heat flow and the gradient. This indicates that the solutions of the heat-conduction equation used in [1-9] do not correspond to the true temperature field. For the solution of the dynamic problems of thermal elasticity we therefore have to employ the new hyperbolic heat-conduction equation derived with consideration of the finite rate of heat propagation [12-15].

Let us consider an elastic half-space at a temperature  $T_0$ ; the temperature field [15] is described by the equation

$$\frac{\partial T(z, t)}{\partial t} + \frac{a}{c_q^2} \frac{\partial^2 T(z, t)}{\partial t^2} = a \frac{\partial^2 T(z, t)}{\partial z^2}. \quad (1)$$

At the instant  $t = 0$  the surface temperature of the half-space varies jumpwise to  $T_c$  and then remains constant. To determine the temperature field we should solve Eq. (1) with the boundary conditions

$$T(z, 0) = T_0, \quad \frac{\partial T(z, 0)}{\partial t} = 0, \quad T(0, t) = T_c. \quad (2)$$

To determine the stresses [16] we have to solve the equation

$$\frac{\partial^2 \sigma_{zz}(z, t)}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2 \sigma_{zz}(z, t)}{\partial t^2} = \frac{1 + \mu}{1 - \mu} \rho \alpha \frac{\partial^2 T(z, t)}{\partial t^2}. \quad (3)$$

We will assume that the half-space is initially free of stresses and that there are no stresses on its surface as the body is heated. The boundary conditions for Eq. (3) will then be

$$\sigma_{zz}(z, 0) = 0, \quad \frac{\partial \sigma_{zz}(z, 0)}{\partial t} = 0, \quad \sigma_{zz}(0, t) = 0. \quad (4)$$

After determining  $\sigma_{zz}$  and  $T$  we can determine the remaining components of the stress tensor easily from [16]:

$$\sigma_{xx} = \sigma_{yy} = \frac{1}{1 - \mu} \{ \mu \sigma_{zz} - E \alpha (T - T_0) \}. \quad (5)$$

Let us introduce the following dimensionless quantities:

$$\sigma = \frac{\sigma_{zz}(1 - 2\mu)}{E \alpha (T_c - T_0)}, \quad \theta = \frac{T - T_0}{T_c - T_0}, \quad \xi = \frac{cz}{a}, \quad \tau = \frac{c^2 t}{a}, \quad M = \frac{c}{c_q}. \quad (6)$$

Lenin Institute of Advanced Machine and Electrical Engineering, Sofia, Bulgaria. Translated from *Inzhenerno-Fizicheskii Zhurnal*, Vol. 16, No. 1, pp. 132-135, January, 1969. Original article submitted July 29, 1968.

© 1972 Consultants Bureau, a division of Plenum Publishing Corporation, 227 West 17th Street, New York, N. Y. 10011. All rights reserved. This article cannot be reproduced for any purpose whatsoever without permission of the publisher. A copy of this article is available from the publisher for \$15.00.

With the aid of (6) we can write Eqs. (1)-(4) in the form

$$\frac{\partial \theta(\xi, \tau)}{\partial \tau} + M^2 \frac{\partial^2 \theta(\xi, \tau)}{\partial \tau^2} = \frac{\partial^2 \theta(\xi, \tau)}{\partial \xi^2}, \quad (7)$$

$$\theta(\xi, 0) = 0, \quad \frac{\partial \theta(\xi, 0)}{\partial \tau} = 0, \quad \theta(0, \tau) = 1, \quad (8)$$

$$\frac{\partial^2 \sigma(\xi, \tau)}{\partial \xi^2} - \frac{\partial^2 \sigma(\xi, \tau)}{\partial \tau^2} = \frac{\partial^2 \theta(\xi, \tau)}{\partial \tau^2}, \quad (9)$$

$$\sigma(\xi, 0) = 0, \quad \frac{\partial \sigma(\xi, 0)}{\partial \tau} = 0, \quad \sigma(0, \tau) = 0. \quad (10)$$

After applying the Laplace transform

$$\bar{\theta}(\xi, s) = \int_0^{\infty} \theta(\xi, \tau) e^{-s\tau} d\tau$$

to Eq. (7), with consideration of the boundary conditions (8) and of the fact that as  $\xi \rightarrow \infty$  the temperature must remain bounded, we find the image of the temperature, i.e.,

$$\bar{\theta}(\xi, s) = \frac{1}{s} \exp[-\xi \sqrt{s(1+M^2s)}]. \quad (11)$$

The reconversion leads to the following relationship:

$$\theta(\xi, \tau) = \eta(\tau - \xi M) \exp\left(-\frac{\xi}{2M}\right) + \frac{\xi}{2M} \int_{\frac{\xi}{2M}}^{\frac{\tau}{2M}} \exp(-x) \frac{I_1\left[\sqrt{x^2 - \left(\frac{\xi}{2M}\right)^2}\right]}{\sqrt{x^2 - \left(\frac{\xi}{2M}\right)^2}} dx, \quad (12)$$

where

$$\begin{aligned} \eta(\tau - \xi M) &= 0 && \text{for } \tau < \xi M, \\ \eta(\tau - \xi M) &= 1 && \text{for } \tau > \xi M. \end{aligned}$$

After application of the Laplace transform

$$\bar{\sigma}(\xi, s) = \int_0^{\infty} \sigma(\xi, \tau) e^{-s\tau} d\tau$$

to Eq. (9), with consideration of the first two conditions in (10), we have

$$\frac{d^2 \bar{\sigma}(\xi, s)}{d\xi^2} - s^2 \bar{\sigma}(\xi, s) = s^2 \bar{\theta}(\xi, s). \quad (13)$$

Having substituted (11) into Eq. (13) and bearing in mind that  $\bar{\sigma}(0, s) = 0$  and that as  $\xi \rightarrow \infty$  the stresses must remain bounded, we find for the images

$$\bar{\sigma}(\xi, s) = \frac{1}{s(1-M^2)-1} [\exp(-\xi s) - \exp[-\xi \sqrt{s(1+M^2s)}]]. \quad (14)$$

Reconversion yields

$$\begin{aligned} \sigma(\xi, \tau) &= \frac{\exp\left(\frac{\tau - \xi}{1-M^2}\right)}{1-M^2} \left\{ \eta(\tau - \xi) - \eta(\tau - \xi M) \exp\left(\frac{\xi}{2M} \frac{M-1}{M+1}\right) \right\} \\ &\quad - \frac{1}{1-M^2} \frac{\xi}{2M} \int_{\xi/2M}^{\tau/2M} \exp\left[-x \frac{1+M^2}{1-M^2}\right] \frac{I_1\left[\sqrt{x^2 - \left(\frac{\xi}{2M}\right)^2}\right]}{\sqrt{x^2 - \left(\frac{\xi}{2M}\right)^2}} dx. \end{aligned} \quad (15)$$

If the heat-propagation rate  $c_q$  is considerably greater than the rate of propagation for the elastic waves, we have  $M = 0$  and the solution coincides with the data in [1] and [4]:

$$\sigma(\xi, \tau) = \eta(\tau - \xi) \exp(\tau - \xi) - \frac{1}{2} e^\tau \left[ e^\xi \operatorname{erfc} \left( \frac{\xi}{2\sqrt{\tau}} + \sqrt{\tau} \right) + e^{-\xi} \operatorname{erfc} \left( \frac{\xi}{2\sqrt{\tau}} - \sqrt{\tau} \right) \right]. \quad (16)$$

#### NOTATION

T	is the temperature;
z	is a coordinate;
t	is the time;
a	is the thermal diffusivity;
$c_q$	is the rate of heat propagation;
$\sigma_{zz}$	is the stress;
c	is the rate of propagation for the elastic waves;
$\mu$	is the Poisson ratio;
$\alpha$	is the coefficient of thermal expansion;
$\rho$	is the mass of the volume unit;
E	is Young's modulus.

#### LITERATURE CITED

1. V. I. Danilovskaya, *Prikl. Matem. i Mekh.*, 14, No. 3 (1950).
2. V. I. Danilovskaya, *Prikl. Matem. i Mekh.*, 16, No. 3 (1952).
3. T. Mura, *Res. Rep. Fac. of Engng., Meiji Univ.*, 7 (1956).
4. T. Mura, *Res. Rep. Fac. of Engng., Meiji Univ.*, 8 (1956).
5. W. Nowacki, *Arch. Mech. Stos.*, 9, 325 (1957).
6. W. Nowacki, *Arch. Mech. Stos.*, 9, 319 (1957).
7. T. Mura, *Proc. Second Japan Nat. Congr. Appl. Mech.* (1952).
8. B. A. Boley and A. D. Barber, *J. Appl. Mech.*, 24, 413 (1957).
9. E. Sternberg and J. G. Charkovorty, *Quart. Appl. Math.*, 17, No. 2, 205 (1959).
10. G. Jaffe, *Ann. Physik*, 6, 195 (1930).
11. G. Jaffe, *Phys. Rev.*, 61, 643 (1942).
12. C. Cattaneo, *Comptes Rendus*, 247, No. 4, 431 (1958).
13. P. Vernote, *Comptes Rendus*, 246, No. 22, 3154 (1958).
14. P. Vernote, *Comptes Rendus*, 247, No. 4 (1959).
15. A. V. Luikov, *Int. J. Heat Mass Transfer*, 9 (1966).
16. H. Parkus, *Instationäre Wärmespannungen*, Springer, Vienna (1959).